

# 2007 2<sup>nd</sup> International Symposium on Wireless Pervasive Computing



**5~7 February 2007  
San Juan, Puerto Rico**

IEEE Catalog Number: 07EX1480  
ISBN: 1-4244-0522-X  
Library of Congress: 2006929656



universidad de puerto rico



Recinto Universitario de **Mayagüez**

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$$\underline{x}[n] = \sum_{j=1}^{K_u} \sum_{k=1}^{N_{sc}} \beta_{jk} \underline{S}_j \otimes \left( \begin{array}{c} (\mathbb{J}^T)^L \mathbb{J}^{l_j} \underline{f}_k[l_j] \underline{S}_j^H (\underline{\gamma}[k] \odot \underline{a}[n-1]) + \\ \mathbb{J}^{l_j} \underline{f}_k[l_j] \underline{S}_j^H (\underline{\gamma}[k] \odot \underline{a}[n]) \\ + (\mathbb{J})^L \mathbb{J}^{l_j} \underline{f}_k[l_j] \underline{S}_j^H (\underline{\gamma}[k] \odot \underline{a}[n+1]) \end{array} \right) + \underline{n}(t) \quad (9)$$

$$\begin{aligned} \underline{x}[n] = & \underbrace{[\mathbf{H}_1 \mathbf{B}_1, \dots, \mathbf{H}_j \mathbf{B}_j, \dots, \mathbf{H}_{K_u} \mathbf{B}_{K_u}] (\underline{1}_{K_u} \otimes \mathbf{C})}_{\mathbb{H}_{desired}} \underline{a}[n] + \\ & \underbrace{[\mathbf{H}_{1,prev} \mathbf{B}_1, \dots, \mathbf{H}_{j,prev} \mathbf{B}_j, \dots, \mathbf{H}_{K_u,prev} \mathbf{B}_{K_u}] (\underline{1}_{K_u} \otimes \mathbf{C})}_{\mathbb{H}_{ISI,prev}} \underline{a}[n-1] + \\ & \underbrace{[\mathbf{H}_{1,next} \mathbf{B}_1, \dots, \mathbf{H}_{j,next} \mathbf{B}_j, \dots, \mathbf{H}_{K_u,next} \mathbf{B}_{K_u}] (\underline{1}_{K_u} \otimes \mathbf{C})}_{\mathbb{H}_{ISI,next}} \underline{a}[n+1] + \underline{n}[n] \end{aligned} \quad (14)$$

a path delay of  $l$  sample periods. In addition,

$$\mathbb{J} = \begin{bmatrix} \mathbb{0}_{2L-1}^T & 0 \\ \mathbb{I}_{2L-1} & \mathbb{0}_{2L-1} \end{bmatrix} \quad (8)$$

is used to model the delay  $l$  on the column vector  $\underline{f}_k$ . For instance, if  $\mathbb{J}^l$  pre-multiplies  $\underline{f}_k$ , it downshifts the elements of  $\underline{f}_k$  by  $l$  elements. On the other hand, pre-multiplying  $\underline{f}_k$  with  $(\mathbb{J}^T)^l$  upshifts the column vector by  $l$  elements. Using  $\underline{f}_k[l]$  and  $\mathbb{J}$  as defined above in Equations 7 and 8, Equation 6 is rewritten as shown in Equation 9.

However, Equation 9 can be further re-expressed as shown in Equation 10.

$$\underline{x}[n] = \sum_{j=1}^{K_u} \left( \begin{array}{c} \mathbf{H}_{j,prev} \mathbf{B}_j \mathbf{C} \underline{a}[n-1] \\ + \mathbf{H}_j \mathbf{B}_j \mathbf{C} \underline{a}[n] \\ + \mathbf{H}_{j,next} \mathbf{B}_j \mathbf{C} \underline{a}[n+1] \end{array} \right) + \underline{n}[n] \quad (10)$$

where

$$\begin{aligned} \mathbf{H}_j &= \underline{S}_j \otimes (\mathbb{J}^{l_j} [\underline{f}_1[l_j], \dots, \underline{f}_k[l_j], \dots, \underline{f}_{N_{sc}}[l_j]]), \quad (11) \\ \mathbf{H}_{j,prev} &= (\mathbb{I}_N \otimes (\mathbb{J}^T)^L) \mathbf{H}_j, \\ \mathbf{H}_{j,next} &= (\mathbb{I}_N \otimes \mathbb{J}^L) \mathbf{H}_j \end{aligned}$$

$$\begin{aligned} \mathbf{B}_j &= \text{diag}(\underline{\beta}_j) \otimes \underline{S}_j^H, \quad (12) \\ \underline{\beta}_j &= [\beta_{j1}, \dots, \beta_{jk}, \dots, \beta_{jN_{sc}}]^T \end{aligned}$$

and

$$\begin{aligned} \mathbf{C} &= [\underline{\gamma}_1 \otimes \underline{e}_1, \dots, \underline{\gamma}_i \otimes \underline{e}_i, \dots, \underline{\gamma}_{\bar{N}} \otimes \underline{e}_{\bar{N}}] \quad (13) \\ &= [\underline{c}_1, \dots, \underline{c}_i, \dots, \underline{c}_{\bar{N}}] \end{aligned}$$

$\underline{c}_i = \underline{\gamma}_i \otimes \underline{e}_i$  and  $\underline{e}_i$  is a  $\bar{N} \times 1$  column vector with 1 at the  $i^{\text{th}}$  position and 0s elsewhere. In Equation 12,  $\mathbf{B}_j$  models the effective fading coefficients on each subcarrier from each antenna element in the transmitter to the reference point of the receiver antenna array. Equation 10 can now be expressed in a vector format in Equation 14. The first term in Equation 14 represents the desired signal component contributed by the current symbol vector, while the second and third terms

represent the ISI components due to the previous and next symbol vectors, respectively.

### C. Receiver Weights Formulation

In this paper, three types of receivers have been considered to compare their relative performances in the proposed system. At point F in Fig. 1, the vector  $\underline{x}[n]$  (from Equation 14) is pre-multiplied by the matrix  $\mathbb{W}^H$  to obtain the decision variable vector  $\underline{d}[n]$ , given by

$$\underline{d}[n] = \mathbb{W}^H \underline{x}[n] \quad (15)$$

The vector  $\underline{d}[n]$  is then multiplexed and passed to the decision device to obtain the received channel symbol stream.

1) *Subspace Based Receiver*: For the proposed subspace based receiver, the channel matrix of the unwanted signals can be formed as

$$\hat{\mathbb{H}}_{ISI} = [\hat{\mathbb{H}}_{ISI,prev} \quad \hat{\mathbb{H}}_{ISI,next}] \quad (16)$$

where  $\hat{\mathbb{H}}_{ISI,prev}$  and  $\hat{\mathbb{H}}_{ISI,next}$  represent the estimates of the ISI components of the previous and next symbols respectively, as given in Equation 14. The complement projection operator of the ISI signal subspace can then be formed by

$$\mathbb{P}_{ISI}^\perp = \mathbb{I}_{2NL} - \hat{\mathbb{H}}_{ISI} (\hat{\mathbb{H}}_{ISI}^H \hat{\mathbb{H}}_{ISI})^{-1} \hat{\mathbb{H}}_{ISI}^H \quad (17)$$

Thus, for the subspace based receiver, the weight matrix,  $\mathbb{W}$ , at point F in Fig. 1, is given by

$$\mathbb{W}_{subspace} = \mathbb{P}_{ISI}^\perp \hat{\mathbb{H}}_{desired} (\hat{\mathbb{H}}_{desired}^H \mathbb{P}_{ISI}^\perp \hat{\mathbb{H}}_{desired})^{-1} \quad (18)$$

$\hat{\mathbb{H}}_{desired}$  represents the estimate of the desired signal component of the current symbol vector.

2) *Minimum Mean Squared Error (MMSE) Receiver*: For the MMSE receiver, the weight matrix,  $\mathbb{W}$ , at point F in Fig. 1, is given by

$$\mathbb{W}_{mmse} = \hat{\mathbb{H}} (\hat{\mathbb{H}}^H \hat{\mathbb{H}} + \sigma_n^2 \mathbb{I}_{2NL})^{-1} \quad (19)$$